**ADA** 

# FISCHER-TROPSCH SYNTHETIC FUEL EVALUATIONS HMMWV TEST TRACK EVALUATION

INTERIM REPORT TFLRF No. 400

by Gregory Hansen Edwin A. Frame

U.S. Army TARDEC Fuels and Lubricants Research Facility Southwest Research Institute® (SwRI®)
San Antonio, TX

by Eric Sattler

for
U.S. Army RDECOM - TARDEC
Force Projection Technologies
Warren, Michigan

**Contract No. DAAE-07-99-C-L053 (WD23)** 

Approved for public release: distribution unlimited

September 2009

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Contract No. DAAE-07-99-C-L053 (WD23) SwRI<sup>®</sup> Project No. 08.03227.23.802

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Steven D. Marty, Director

U.S. Army TARDEC Fuels and Lubricants

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#### **EXECUTIVE SUMMARY**

This test utilizes a HMMWV in comparing four different fuels. Evaluation criteria include fuel economy, emissions, vehicle performance, and engine wear. In general, when the HMMWV was running on DF-2 fuel, performance characteristics were the highest, emissions levels were the highest, and fuel economy was the highest. On the other end of the spectrum was the Fischer-Tropsch S-8 fuel. HMMWV performance with S-8 or the fuel blend was reduced in comparison to DF-2. Fuel economy suffered, largely in part to a decreased volumetric energy density, and different combustion characteristics. However, emissions levels were lower for S-8 fuel than any of the others. Again, speaking generally, the 50/50 blend of JP-8 and S-8 vehicle performance and other characteristics fell in the middle of the JP-8 and S-8 fuels.

#### FOREWORD/ACKNOWLEDGMENTS

The U.S. Army TARDEC Fuel and Lubricants Research Facility (TFLRF) located at Southwest Research Institute (SwRI), San Antonio, Texas, performed this work during the period of January 2009 through September 2009 under Contract No. DAAE-07-99-C-L053. The U.S. Army Tank-Automotive RD&E Center, Force Projection Technologies, Warren, Michigan administered the project. Mr. Luis Villahermosa (AMSRD-TAR-D/MS110) served as the TARDEC contracting officer's technical representative. Ms. Pat Muzzell and Mr. Eric Sattler of the U.S. Army National Automotive Center served as project technical monitors.

The authors would also like to recognize the contribution of Jeff Sellers for his technical support and dedication. Finally, thanks to the administrative and report-processing support provided by Dianna Barrera.

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#### **APPENDIX**

VIDEO – Testing of "HMMWV Fuel Comparison"

Use the following link to access the video:

 $\underline{http://www.swri.org/4org/d02/Reports/Misc/HMMWVFuelComp.wmv}$ 

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#### ACRONYMS AND ABBREVIATIONS

% Percent

°C Degrees centigrade °F Degrees Fahrenheit

@ At

ASTM American Society for Testing and Materials

bhp Brake horsepower
BTU British thermal units
cc cubic centimeter
cm centimeter

CO Carbon monoxide cSt Centistokes

cSt Centisto deg degree

DOD Department of Defense
FBP Final boiling point
FTM Federal Test Method
FTP Federal Test Procedure
g/kw-h Grams per kilowatt-hour

g/mi Grams per mile

GEP General Engine Products

GFM Government furnished equipment

GVW Gross Vehicle Weight

HC Hydro-Carbon

HFRR High-frequency reciprocating rig

Hr Hour

HMMWV High Mobility Medium Wheeled Vehicle

IBP Initial boiling point

Kg Kilo-gram
L Liter
Lbs Pounds
Max Maximum
mg Milligram

mg/l Milligrams per liter

mgKOH/g Milligrams potassium hydroxide per gram of sample

Min Minimum

MJ/Kg Megajoules per kilogram

ml Milliliter mm Millimeter

mmHG Millimeters of mercury

MPG Miles per gallon

N No

NOx Oxides of nitrogen NR Not required

oz Ounce

PM Particulate matter ppm Parts per million

psi pounds per square inch RPM Revolutions per minute

S, sec Seconds

SLBOCLE Scuffing load ball on cylinder lubricity evaluator

SPK Synthetic Paraffinic Kerosene

STDEV Standard deviation

SwRI Southwest Research Institute

TFLRF U.S. Army TARDEC Fuels and Lubricants Research Facility

THC Total hydrocarbons
ULSD Ultra-Low Sulfur Diesel

um micrometer V Voltage

WOT Wide open throttle

Wt. Weight Y Yes

1.0 BACKGROUND AND OBJECTIVES

**BACKGROUND** 

Fischer-Tropsch (F-T) process synthetic fuels, first produced in 1927, were used by WWII

Germany, and by South Africa during their embargoed period, to overcome petroleum shortages.

Synthetic JP-8 is a clean fuel that contains no sulfur or aromatics, but has historically cost too

much to compete with petroleum fuel. Since the mid-1990s, the world's major energy companies

have begun developing updated F-T processes that are less expensive to build and operate.

However, synthetic fuel chemistry differs significantly from petroleum fuels since F-T synthetic

fuels are free of aromatic and sulfur compounds. The U.S. Military needs to understand the

extent and nature of these differences and the implications regarding current and future military

use. There will be some subtle and not so subtle changes in fuel compositions and associated

physicochemical properties that can impact engine performance and durability. The U.S. Army

Synthetic fuels project will involve assessments of the impacts that varying fuel properties may

have on current and future military equipment and systems.

**OBJECTIVES** 

This test will specifically measure the performance, emissions, fuel economy, and compare

engine wear for four (4) different fuels.

**APPROACH** 

A HMMWV will be instrumented and run in field-like conditions. With 200 miles being

accumulated on each of the four (4) fuels. The HMMWV will also be evaluated on a test track

for repeatable performance data.

2.0 TEST EVALUATION

**FUELS** 

The four (4) fuels are: DF-2 ULSD, JP-8, F-T S-8 [SPK], 50/50 (volume) Blend of S-8 and JP-8.

The fuel properties are found in Table 1.

1

Table 1. Fuel Properties for ULSD, JP-8, 50/50 Blend, and S-8

| Property                        | ASTM D   | DF-2           | JP-8            | 50/50 Blend     | S-8  |
|---------------------------------|----------|----------------|-----------------|-----------------|--|
| Description                     |          | ULSD           | Age<br>Refining | DCI-4a          | w/ 22.5 ppm<br>DCI-4a<br>Iubricity<br>enhancer |
| Density @ 15 C [kg/L]           | 4052     | 0.8556         | 0.7931          | 0.7739          | 0.7554   |
| API Gravity @ 15 C              | 4052     | 34.2           | 47.4            | 51.3            | 55.8   |
| TAN [mg KOH/g]                  | 3242     |                | 0.010           | 0.010           | <0.001   |
| Aromatics [vol %]               | 1319     | 28.1           | 15.2            | 8               | 0.5  |
| Total Sulfur [ppm]              | see note | 8 <sup>1</sup> | 90²             | 38 <sup>2</sup> | <13  |
| Distillation [deg C @ vol %]    |          |                |                 |                 |  |
| IBP                             |          | 172            | 144             | 149             | 165  |
| 10                              |          | 215            | 164             | 164             | 173  |
| 20                              |          | 228            | 170             | 168             | 176  |
| 50                              | 86       | 264            | 192             | 195             | 205  |
| 90                              |          | 317            | 245             | 249             | 256  |
| FBP                             |          | 346            | 265             | 271             | 277  |
| residue                         |          | 1.1            | 1.5             | 1.5             | 1.6  |
| loss                            |          | 2.8            | 1.3             | 1.1             | 1.2  |
| Viscosity @ 40 C [cm^2/s]       | 445      | 2.60           | 1.10            | 1.21            | 1.35   |
| Net Heat of Combustion [BTU/Lb] | 3338     | 18,425         | 18,663          | 18,807          | 18,975   |
| Hydrogen Content [mass %]       | 3343     | 13.37          | 14.06           | 14.65           | 15.37  |
| Cetane Number                   | 613      | 47.5           | 46.0            | 53.0            | 62.7   |
| Calculated Cetane Index         | 4737     | 46.1           | 45.0            | 55.3            | 64.4   |
| BOCLE [mm]                      | 5001     | 0.67           | 0.48            | 0.50            | 0.56   |
| HFRR [um]                       | 6079     | 610            | 720             | 723             | 819  |

<sup>&</sup>lt;sup>1</sup> ASTM D5453

#### **EQUIPMENT**

Test vehicle: GFE HMMWV (See Figure 1)

S/N: 180209Year: 1998

• Engine: GEP 6.5L V8 Diesel, naturally aspirated

• Driveline: 4-speed transmission, 2-speed transfer case

<sup>&</sup>lt;sup>2</sup> ASTM D2622

<sup>&</sup>lt;sup>3</sup> ASTM D3227

#### Measurement Devices:

- AVL smoke meter
- Cambell Data Acquisition for engine operating conditions
- Daytron Data Aacquision for vehicle dynamics
- Sensors Inc. Portable Emissions Monitoring System



Figure 1. HMMWV Used for Testing

#### **EQUIPMENT PREPARATION**





Figure 2. Ballast on Front and Rear of the HMMWV

The HMMWV was modified to accept the PEMS unit on the exhaust. A rack was installed in the bed of the HMMWV to accept concrete ballast. To maintain even weight distribution a rack for additional weights was installed on the front bumper; see Figure 2. The remaining data acquisition systems were installed as appropriate; see Figure 3. Not all of the measurement systems were on the vehicle during each phase of the test. The vehicle's power system and available space were constraints that limited the use of the measurement systems.



Figure 3. Some Instrumentation on the HMMWV

#### **TEST PROCEDURE**

The test plan followed this generalized format:

- Fill with test fuel
- Drive 100 miles unballasted
- Measure fuel consumed
- Perform acceleration tests with emissions unballasted
- Ballast to 10,300 Lbs

- Perform acceleration tests with emissions
- Perform engine start tests [beginning of day for consistency]
- Refill with test fuel
- Drive 100 miles ballasted
- Measure fuel consumed
- Perform smoke tests
- Take oil samples
- Repeat

#### **TEST ROUTE**

The test route is shown in red [with number markers] on Figure 4. The vehicle starts the 100 mile segment from the fleet lab. The vehicle drives to the test track [marker 2] and performs 8 laps. The vehicle then follows the route [numbers 4 through 8] in order. The route continues from marker 8 to marker 1 and on until the 100 miles is completed.



Figure 4. Driving Route on SwRI Campus

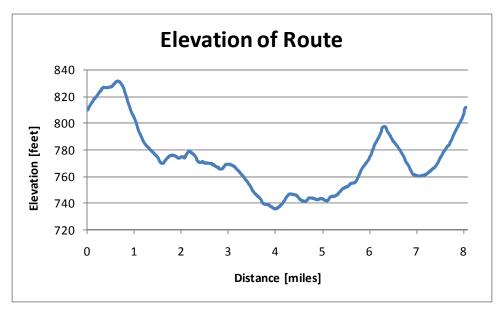


Figure 5. Elevation Change of Driving Route on SwRI Campus

Marker 2 on the aerial map [mile 2 on Figure 4] indicates the test track. During actual testing the vehicle performed eight laps on the test track every time around the course. The elevation change was as large as possible while still staying on SwRI campus, see Figure 5 above.

#### 3.0 DISCUSSION OF RESULTS AND COMPARISONS

The first S-8 run will not be included because the data is not consistent. There was a learning curve in operating this test. The average MPH was a little low, so the driver was instructed to increase speed around the paved test track (from 40 to 45 MPH). This caused a change in the fuel economy. The video and photography also interfered with the fuel economy as the vehicle was idling and/or off for some time during the scheduled 100 mile accumulation periods. Furthermore, the test was initiated before the reconditioning of the procured smoke meter was finished. This precluded gathering smoke samples from the first S-8 testing period.

#### **ECONOMY**

The fuel density was measured according to ASTM D4052.

**Table 2. Indicated Fuel Economy Data** 

| Fuel Type        | Ballasted to GVW (Y/N)     | Miles      | Weight Consumed lbs | Fuel Density kg/L | MPG   |
|------------------|----------------------------|------------|---------------------|-------------------|-------|
| S8*              | N                          | 100        | 51.30               | 0.7554            | 12.29 |
| S8               | Υ                          | 100        | 64.30               | 0.7554            | 9.80  |
| DF2              | N                          | 100        | 57.50               | 0.8556            | 12.42 |
| DF2              | Υ                          | 100        | 64.00               | 0.8556            | 11.16 |
| JP8              | N                          | 100        | 55.80               | 0.7931            | 11.86 |
| JP8              | Υ                          | 100        | 67.60               | 0.7931            | 9.79  |
| 50/50            | N                          | 100        | 55.50               | 0.7739            | 11.64 |
| 50/50            | Υ                          | 100        | 60.80               | 0.7739            | 10.62 |
| S8               | N                          | 100        | 58.71               | 0.7554            | 10.74 |
| S8               | Υ                          | 100        | 61.90               | 0.7554            | 10.18 |
| * track speed li | mit 5 mph less than all of | ther tests |                     |                   |       |

The fuel economy results seen in Table 2, show decreased values starting with DF2 and ending with S-8. This correlates well with expected results based on fuel energy density, cetane number, and viscosity differences among the fuel types.

For comparison it is useful to look at the percent difference between the average MPG and other engine operating parameters for each 100 mile segment, as shown in Table 3 and 4.

**Table 3. Comparison of Indicated Fuel Economy** 

|                  | Ballasted to |       | % Change with     | % Change with   | Average |
|------------------|--------------|-------|-------------------|-----------------|---------|
| <b>Fuel Type</b> | GVW (Y/N)    | MPG   | JP8 as a Baseline | DF2 as Baseline | MPH     |
| DF2              | N            | 12.42 | 4.5%              | n/a             | 27.73   |
| DF2              | Υ            | 11.16 | 13.9%             | n/a             | 26.12   |
| JP8              | N            | 11.86 | n/a               | -4.5%           | 27.52   |
| JP8              | Υ            | 9.79  | n/a               | -12.2%          | 25.13   |
| 50/50            | N            | 11.64 | -1.9%             | -6.3%           | 26.27   |
| 50/50            | Υ            | 10.62 | 8.5%              | -4.8%           | 26.44   |
| S8               | N            | 10.74 | -9.5%             | -13.5%          | 26.28   |
| S8               | Υ            | 10.18 | 4.0%              | -8.7%           | 26.87   |

If JP-8 is a baseline fuel for comparison, the S-8 lost up to 9.5% fuel economy.

**Table 4. 100 Mile Engine Operation Summary Data** 

|                  |           |       | Averages |                    |         |      |  |
|------------------|-----------|-------|----------|--------------------|---------|------|--|
|                  | Ballasted |       | Oil Sump | <b>Coolant Out</b> | Ambient |      |  |
| <b>Fuel Type</b> | (Y/N)     | Miles | Temp F   | Temp F             | Temp F  | RPM  |  |
| DF2              | N         | 100   | 184.0    | 200.0              | 77.3    | 1487 |  |
| DF2              | Υ         | 100   | 176.5    | 199.9              | 73.7    | 1446 |  |
| JP8              | N         | 100   | 175.0    | 197.9              | 68.0    | 1452 |  |
| JP8              | Υ         | 100   | 171.4    | 198.0              | 68.8    | 1431 |  |
| 50/50            | N         | 100   | 177.6    | 197.7              | 71.7    | 1397 |  |
| 50/50            | Υ         | 100   | 186.0    | 200.8              | 93.2    | 1443 |  |
| S8               | N         | 100   | 180.2    | 199.2              | 73.3    | 1408 |  |
| S8               | Υ         | 100   | 178.6    | 199.9              | 80.1    | 1479 |  |

There is, however, no single measured variable responsible for the observed fuel economy differences

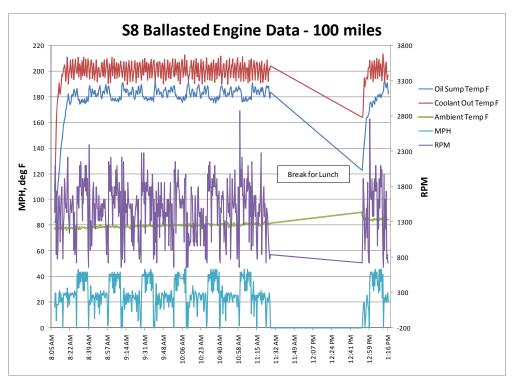


Figure 6. Time Resolved Example Data: Showing 100 Miles of Driving on S8 Fuel with the HMMWV
Ballasted to 10,300 Lbs

Figure 6 shows vehicle operating conditions for one day, or 100 miles of testing. The data presented is for the S-8 fuel with the vehicle ballasted.

#### **ACCELERATION**

The ½ mile test track has an approximate 1 percent slope from beginning to end. This accounts for the uphill/downhill distinction seen in the reported performance and emissions. Table 5 consists of 5 runs in each direction and the averages of each run, from 0 to 50 MPH, are presented.

Table 5. 5 Run Averaged Acceleration Data

| Acceleration 0 to 50 MPH            |           |          | DF2  | JP8  | 50/50 | S8   |
|-------------------------------------|-----------|----------|------|------|-------|------|
|                                     | Ballasted | Uphill   | 22.1 | 28.5 | 30.9  | 33.8 |
| Average Time                        | Dallasteu | Downhill | 20.3 | 23.8 | 28.9  | 29.4 |
| [seconds]                           | Empty     | Uphill   | 15.1 | 16.1 | 18.5  | 18.1 |
|                                     | ЕШРІУ     | Downhill | 13.6 | 14.7 | 17.0  | 16.7 |
| Average                             | Ballasted | Uphill   | 1057 | 1388 | 1515  | 1671 |
| Distance                            | Dallasteu | Downhill | 988  | 1153 | 1438  | 1469 |
| [feet]                              | Empty     | Uphill   | 708  | 756  | 887   | 845  |
| [leet]                              |           | Downhill | 645  | 687  | 814   | 791  |
| Λνοτασο                             | Ballasted | Uphill   | 3.31 | 2.57 | 2.37  | 2.17 |
| Average<br>Acceleration<br>[ft/s^2] | Dallasteu | Downhill | 3.62 | 3.08 | 2.54  | 2.49 |
|                                     | Empty     | Uphill   | 4.37 | 3.93 | 3.67  | 3.51 |
|                                     |           | Downhill | 4.64 | 4.32 | 3.71  | 3.79 |

The data may also be seen in Table 6, with JP-8 as a baseline for easy comparison. A positive percentage value means: a faster time, a shorter distance, and a larger acceleration.

Table 6. Comparison of Averaged Acceleration Data

| Acceleration 0 to 50 MPH |           |          | DF2   | JP8  | 50/50  | S8     |
|--------------------------|-----------|----------|-------|------|--------|--------|
|                          | Ballasted | Uphill   | 22.3% | 0.0% | -8.4%  | -18.4% |
| Avorago Timo             |           | Downhill | 15.0% | 0.0% | -21.4% | -23.6% |
| Average Time             | Empty     | Uphill   | 6.6%  | 0.0% | -14.5% | -12.3% |
|                          | ЕШРІУ     | Downhill | 7.8%  | 0.0% | -15.9% | -13.9% |
|                          | Ballasted | Uphill   | 23.8% | 0.0% | -9.1%  | -20.3% |
| Average                  |           | Downhill | 14.3% | 0.0% | -24.7% | -27.4% |
| Distance                 | Empty     | Uphill   | 6.4%  | 0.0% | -17.3% | -11.8% |
|                          |           | Downhill | 6.1%  | 0.0% | -18.4% | -15.1% |
|                          | Ballasted | Uphill   | 28.6% | 0.0% | -7.8%  | -15.5% |
| Average                  | Ballasteu | Downhill | 17.4% | 0.0% | -17.7% | -19.1% |
| Acceleration             | Empty     | Uphill   | 11.2% | 0.0% | -6.6%  | -10.6% |
|                          | Empty     | Downhill | 7.4%  | 0.0% | -14.0% | -12.3% |

Consistent trends come from the HMMWV configuration running uphill and ballasted. With JP-8 as the baseline for this configuration, vehicle performance was degraded up to 9% running on the 50/50 blend and up to 20% running the full S-8.

The most telling data of all is the 58% increase in distance traveled from 0 to 50 MPH if the vehicle is ballasted, running uphill, and the fuels compared are DF2 and S-8.

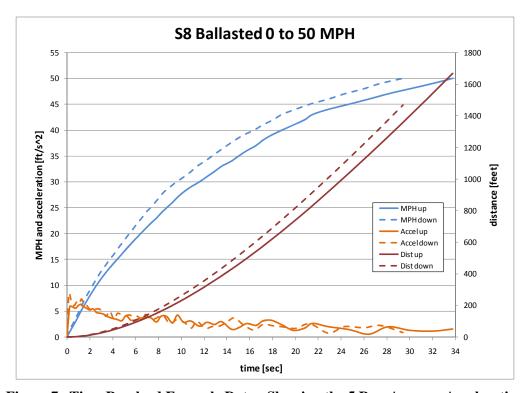


Figure 7. Time Resolved Example Data: Showing the 5 Run Average Acceleration
Data from Driving on S8 Fuel with the HMMWV
Ballasted to 10,300 Lbs

Figure 7 shows the time resolved vehicle dynamics from two 5 run averages accelerating from 0 to 50 MPH. The vehicle configuration is ballasted and running S-8 fuel.

#### **EMISSIONS AND SMOKE**

Emissions data are presented from the acceleration runs of 0 to 50 MPH in Table 7.

Table 7. 5 Run Averaged Emissions Data

| Emissions 0 to 50 MPH |           |          | DF2   | JP8   | 50/50 | S8    |
|-----------------------|-----------|----------|-------|-------|-------|-------|
|                       | Ballasted | Uphill   | 166.2 | 146.0 | 133.0 | 121.6 |
| Average CO            | Dallasteu | Downhill | 175.2 | 145.0 | 134.0 | 124.9 |
| [ppm]                 | Empty     | Uphill   | 193.5 | 85.5  | 147.8 | 165.5 |
|                       | Empty     | Downhill | 189.5 | 131.8 | 153.5 | 167.1 |
|                       | Ballasted | Uphill   | 449.3 | 446.8 | 328.1 | 296.2 |
| Average NOx           | Dallasteu | Downhill | 454.2 | 443.4 | 329.4 | 294.6 |
| [ppm]                 | Empty     | Uphill   | 453.6 | 456.5 | 324.1 | 297.6 |
|                       |           | Downhill | 460.0 | 459.7 | 318.3 | 296.6 |
|                       | Ballasted | Uphill   | 6.2   | 8.1   | 16.6  | 12.2  |
| Average HC            | Dallasteu | Downhill | 9.2   | 9.5   | 14.5  | 11.4  |
| [ppm]                 | F         | Uphill   | 11.3  | 17.9  | 25.1  | 18.4  |
|                       | Empty     | Downhill | 10.4  | 13.6  | 23.8  | 12.7  |

Emissions quality generally improves when moving to the S-8 fuel.

Again it is useful to look at the data on an improvement basis with JP-8 as a baseline, as shown in Table 8. A positive percentage indicates a lower emissions level.

Table 8. Comparison of the 5 Run Averaged Emissions Data

| Emissions 0 to 50 MPH |           |          | DF2     | JP8  | 50/50   | S8     |
|-----------------------|-----------|----------|---------|------|---------|--------|
|                       | Ballasted | Uphill   | -13.8%  | 0.0% | 8.9%    | 16.7%  |
| Average CO            | Dallasteu | Downhill | -20.8%  | 0.0% | 7.6%    | 13.8%  |
| Average CO            | Empty     | Uphill   | -126.5% | 0.0% | -72.9%  | -93.7% |
|                       | Empty     | Downhill | -43.8%  | 0.0% | -16.5%  | -26.8% |
|                       | Ballasted | Uphill   | -0.6%   | 0.0% | 26.6%   | 33.7%  |
| Average NOx           | Dallasteu | Downhill | -2.4%   | 0.0% | 25.7%   | 33.6%  |
| Average NOX           | Empty     | Uphill   | 0.7%    | 0.0% | 29.0%   | 34.8%  |
|                       |           | Downhill | -0.1%   | 0.0% | 30.8%   | 35.5%  |
|                       | Ballasted | Uphill   | 23.4%   | 0.0% | -106.4% | -51.7% |
| Average HC            | Ballasteu | Downhill | 2.7%    | 0.0% | -53.1%  | -19.7% |
|                       | Empty     | Uphill   | 36.6%   | 0.0% | -40.5%  | -2.8%  |
|                       |           | Downhill | 23.5%   | 0.0% | -75.1%  | 6.7%   |

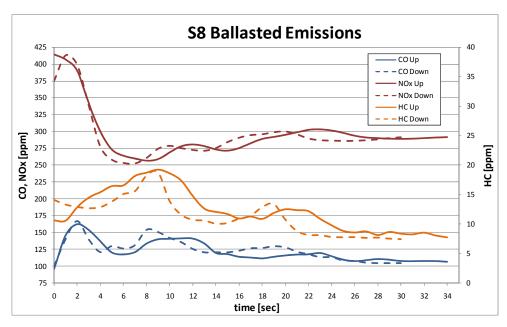


Figure 8. Time Resolved Example Data: Showing the 5 Run Average Emissions
Data from Driving on S8 Fuel with the HMMWV
Ballasted to 10,300 Lbs

Figure 8 shows the time resolved emissions from two 5 run averages accelerating from 0 to 50 MPH. The vehicle configuration is ballasted and running S-8 fuel.

The smoke data is presented, in Table 9, on a volumetric basis for ease of comparison. The measurements were made by the AVL smoke meter by sampling the exhaust gas for a specific length of time and then reading the sample according to the Bosch smoke procedure. The values presented represent the average of 3 runs at each condition. For the first condition, the HMMWV engine was on and the transmission was in neutral. For the second condition, the HMMWV was traveling at a constant 30 MPH in high gear. For the third condition, the smoke sample was taken while the vehicle was accelerating under WOT from 0 to 50 MPH. The fourth condition shows the bias with the engine off.

Table 9. 3 Run Averaged Smoke Data

|                                  |           |             | DF2   | JP8  | 50/50 | S8   |
|----------------------------------|-----------|-------------|-------|------|-------|------|
| Average Smoke [mg/m^3] Ballasted | Idle      | 0.54        | 1.29  | 0.85 | 0.74  |      |
|                                  | Dallastad | 30 MPH      | 2.25  | 2.83 | 2.44  | 2.26 |
|                                  | Ballasteu | WOT 0 to 50 | 35.91 | 9.70 | 9.48  | 6.85 |
|                                  |           | Off         | 0.14  | 0.08 | 0.01  | 0.06 |

Overall the S-8 showed slightly less smoke than the JP8, while the DF2 showed a high volume of smoke.

#### **START TIMES**

The cold start times are one measurement, not an average. They were performed at the beginning of the day to ensure consistency, as shown in Table 10. The hot start times were performed after the engine oil was brought up to operating temperature.

**Table 10. Indicated Start Times** 

|            |      | DF2  | JP8  | 50/50 | S8   |
|------------|------|------|------|-------|------|
| Start Time | Hot  | 0.40 | 0.40 | 0.60  | 0.50 |
| [seconds]  | Cold | 0.65 | 0.80 | 0.80  | 1.00 |

Generally the S-8 showed longer start times than the JP-8 or DF2.

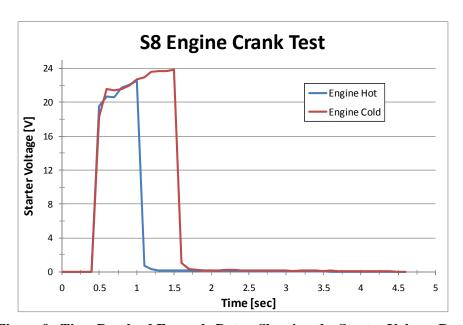


Figure 9. Time Resolved Example Data: Showing the Starter Voltage Data from Running on S8 Fuel

Figure 9 shows the time resolved starter voltage for the hot and cold engine conditions. The vehicle is running S-8 fuel.

#### **OIL ANALYSIS**

The oil analysis, as seen in Table 11 shows essentially no differences in engine wear or oil degradation. There was no measurable fuel dilution, or soot dilution. The key wear metals showed no more than a single digit increase. Finally, the oil's acid number showed no increase.

Table 11. Results of Oil Analysis

|   | New Oil | DF-2   | JP-8   | 50/50  | S-8    |
|---|---------|--------|--------|--------|--------|
| ASTM D3524M Fuel Dilution Diesel (wt.%) | NA      | < 0.3  | < 0.3  | < 0.3  | < 0.3  |
| ASTM D445 Viscosity @ 100°C (cSt)       | 14.62   | 14.50  | 14.38  | 14.39  | 14.40  |
| ASTM D445 Viscosity @ 40°C (cSt)        | 110.03  | 109.20 | 108.34 | 108.50 | 108.28 |
| ASTM D4739 Total Base Number            |         |        |        |        |        |
| Inflection Point (mg KOH/g)             | 8.36    | 7.85   | 8.17   | 8.43   | 8.64   |
| ASTM D4739 Total Base Number            |         |        |        |        |        |
| Buffer Point (mg KOH/g)                 | 8.31    | 7.78   | 7.88   | 8.17   | 9.02   |
| ASTM D5185 Elemental Analysis (ppm)     |         |        |        |        |        |
| Aluminum (Al)                           | <1      | 1      | 1      | 1      | 1      |
| Antimony (Sb)                           | <1      | <1     | <1     | <1     | <1     |
| Barium (Ba)                             | <1      | <1     | <1     | <1     | <1     |
| Boron (B)                               | 5       | 3      | 4      | 3      | 4      |
| Calcium (Ca)                            | 2595    | 2659   | 2719   | 2689   | 2680   |
| Chromium (Cr)                           | <1      | <1     | <1     | <1     | <1     |
| Copper (Cu)                             | <1      | <1     | <1     | <1     | <1     |
| Iron (Fe)                               | 2       | 6      | 6      | 4      | 4      |
| Lead (Pb)                               | <1      | <1     | <1     | <1     | <1     |
| Magnesium (Mg)                          | 12      | 8      | 14     | 10     | 12     |
| Manganese (Mn)                          | <1      | <1     | <1     | <1     | <1     |
| Molybdenum (Mo)                         | 2       | 2      | 3      | 2      | 2      |
| Nickel (Ni)                             | <1      | <1     | <1     | <1     | <1     |
| Phosphorus (P)                          | 1054    | 1049   | 1056   | 1042   | 1036   |
| Silicon (Si)                            | 4       | 2      | 5      | 3      | 3      |
| Silver (Ag)                             | <1      | <1     | <1     | <1     | <1     |
| Sodium (Na)                             | 6       | 5      | 5      | 5      | 5      |
| Tin (Sn)                                | <1      | <1     | <1     | <1     | <1     |
| Zinc (Zn)                               | 1191    | 1212   | 1225   | 1206   | 1203   |
| Potassium (K)                           | 6       | 5      | 7      | 6      | 6      |
| Strontium (Sr)                          | <1      | <1     | <1     | <1     | <1     |
| Vanadium (V)                            | <1      | <1     | <1     | <1     | <1     |
| Titanium (Ti)                           | <1      | <1     | <1     | <1     | <1     |
| Cadmium (Cd)                            | <1      | <1     | <1     | <1     | <1     |
| ASTM D664 Total Acid Number             |         |        |        |        |        |
| Buffer Point (mg KOH/g)                 | 2.2     | 1.99   | 2.14   | 2.16   | 2.19   |
| TGA Soot (wt.%)                         | 0.125   | 0.136  | 0.190  | 0.109  | 0.159  |

#### 4.0 CONCLUSIONS

When JP-8 is used as a baseline for comparison, the S-8 fuel performed worse in vehicle dynamics, but performed better in emissions. The results of the 50/50 blend of JP8 and S-8 fell right in between the results of the 2 constituent fuels.

The engine oil tests showed no significant wear during the 200+ miles of testing. In total the HMMWV accumulated 1652 miles. Only 1000 of those miles are accounted for by the fuel economy testing. The remaining 652 miles largely consisted of the acceleration tests which may be characterized by WOT engine operation and hard braking. The fuel pump was analyzed by a local calibration facility. As a result of the testing, the pump showed very little wear. This is the reason the calibration tables were not included in the body of the report. The pump calibration tables are found in the appendix.

#### 5.0 RECOMMENDATIONS

TLFRF staff is very confident in the vehicle performance and emissions data. The cold start and hot start data cannot be interpreted with a high level of confidence, since there is only one data point per fuel used. If a more confident data set is required a specialized set of cold start tests is recommended.

Similarly, the fuel economy can only be viewed as an indication of results. Repeatability is required for fuel economy comparison, and the scope of this test did not include repeated 100 mile fuel economy segments.

Longer term effects of S-8 fuel use should be investigated.

### **APPENDIX A**

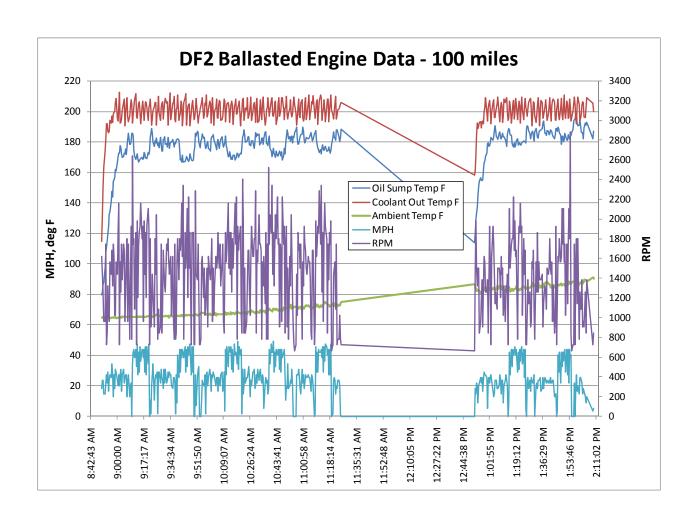
## Fischer-Tropsch Synthetic Fuels Evaluations HMMV Test Track Evaluation

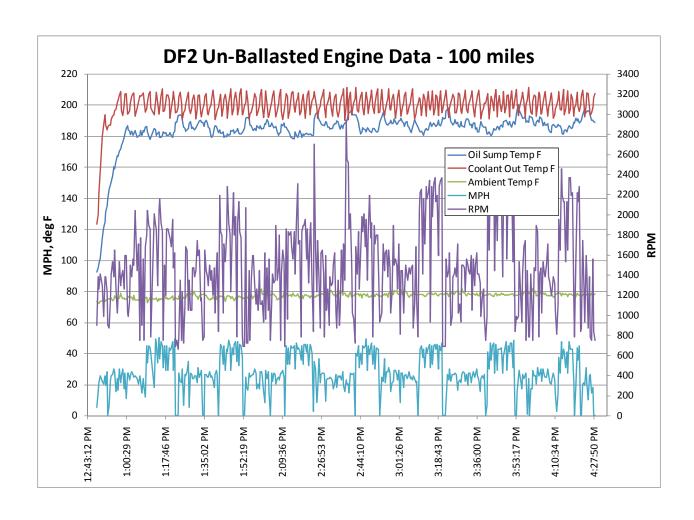
Work Directive No. 23, Task XI

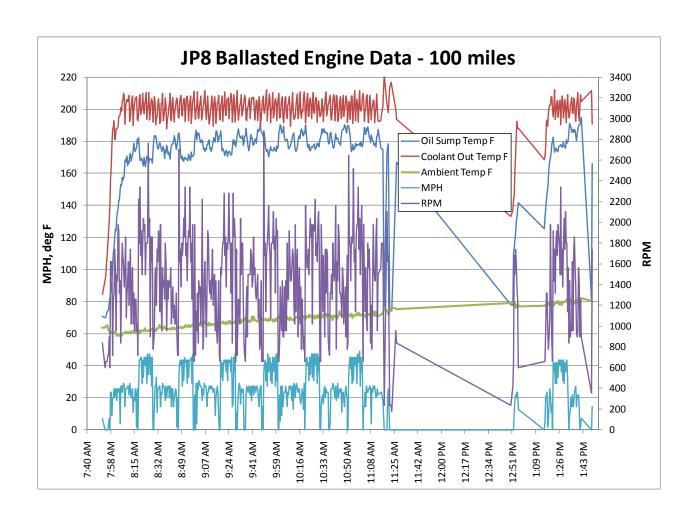
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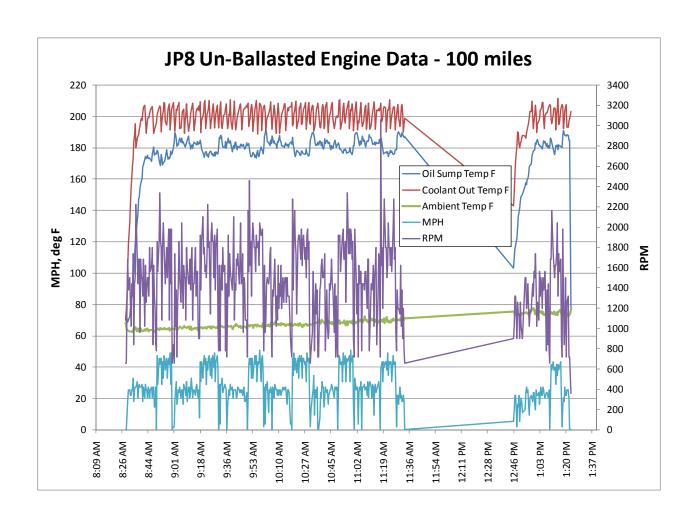
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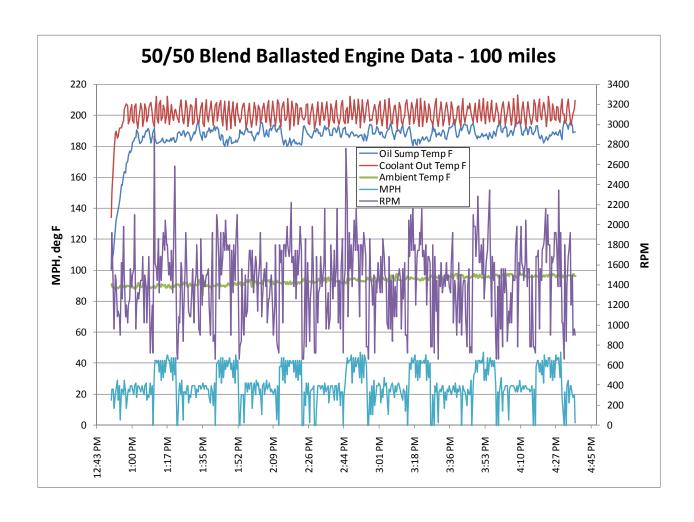
U.S. Army TARDEC Force Projection Technologies Warren, Michigan 48397-5000

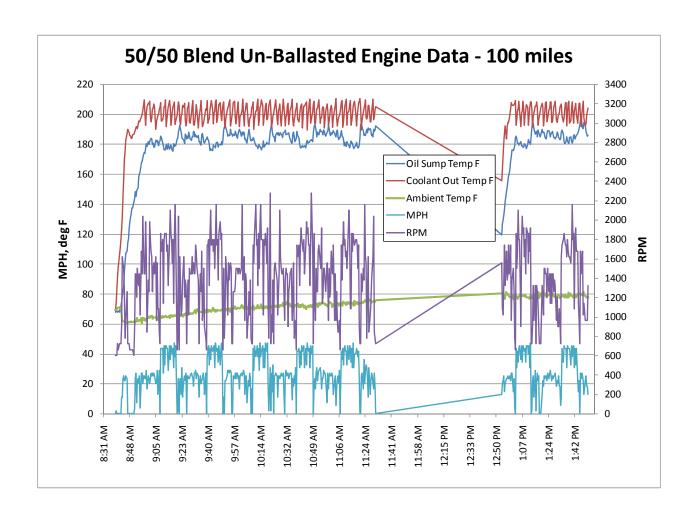


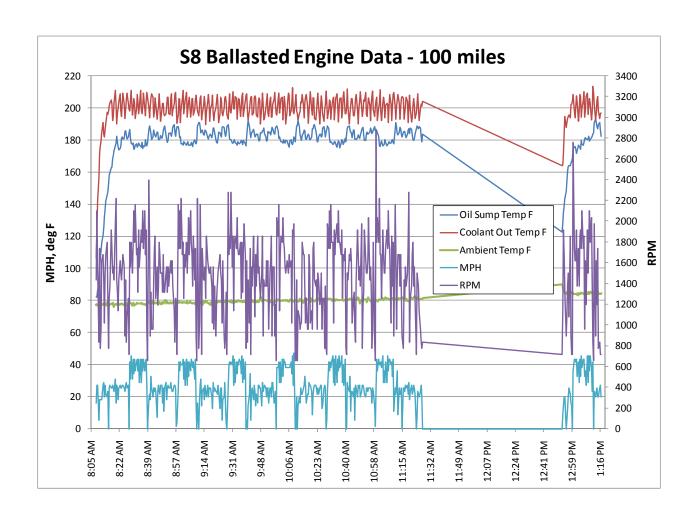


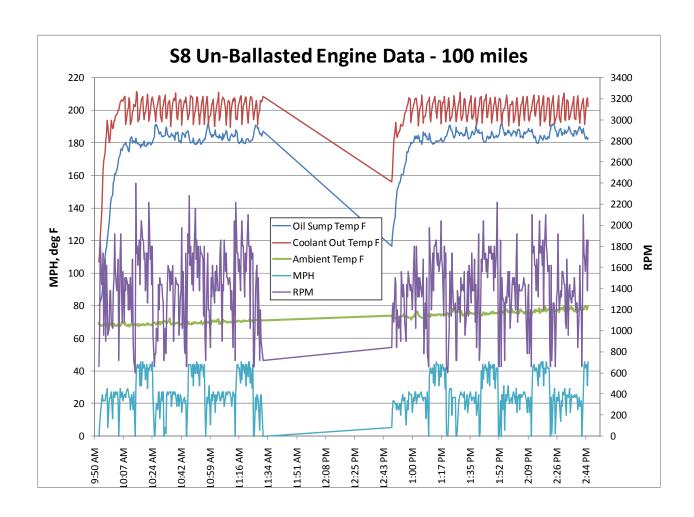












### **APPENDIX B**

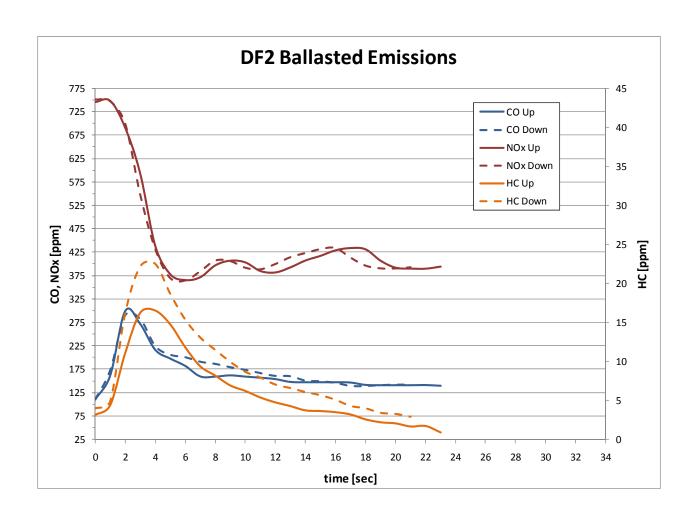
## Fischer-Tropsch Synthetic Fuels Evaluations HMMV Test Track Evaluation

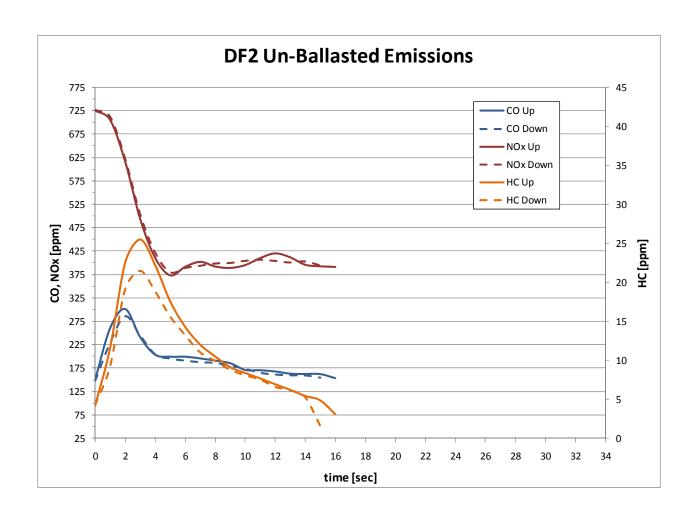
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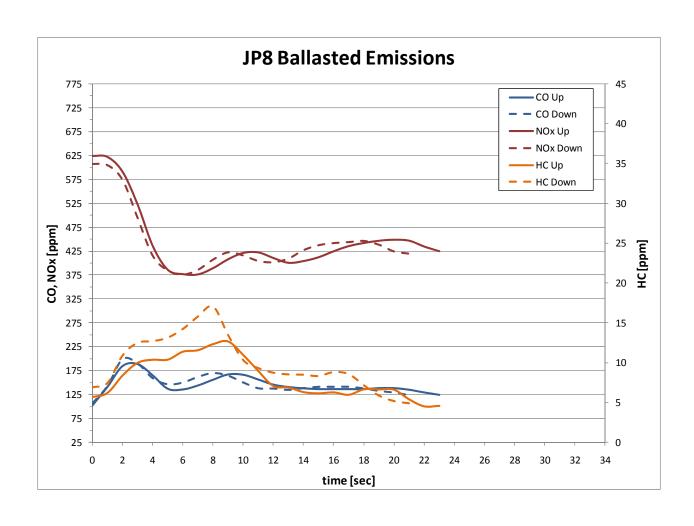
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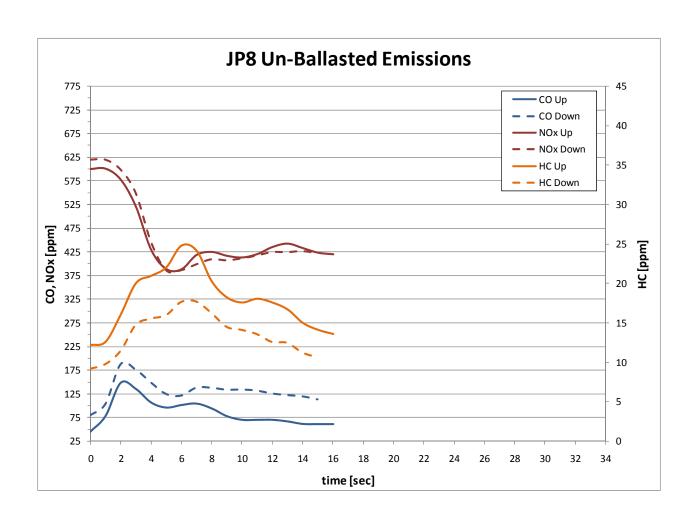
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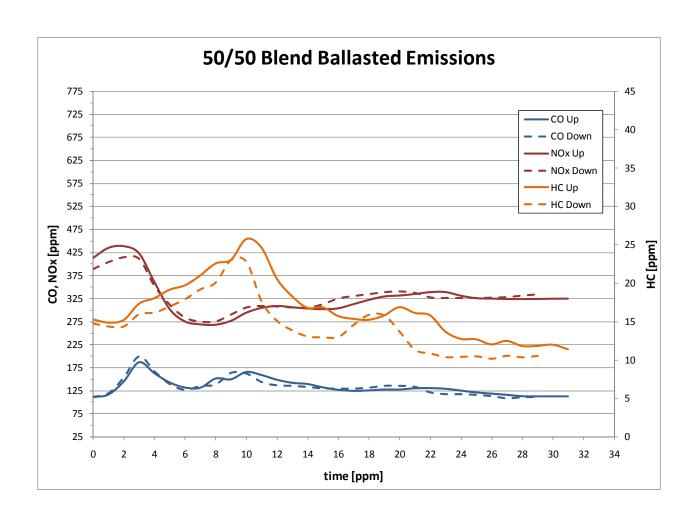
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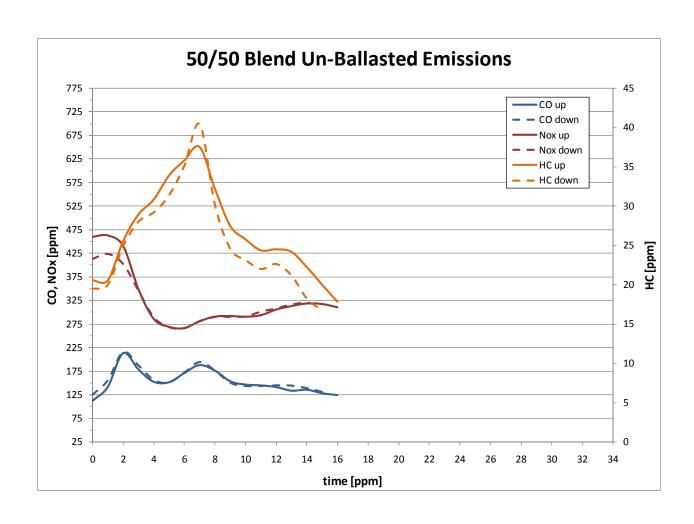


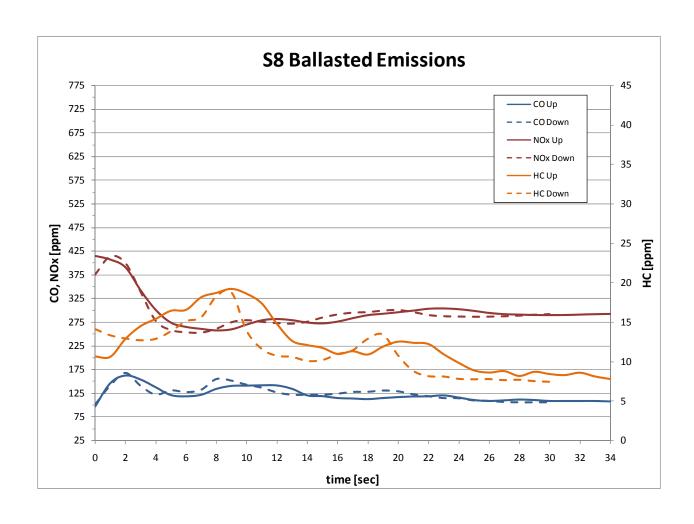


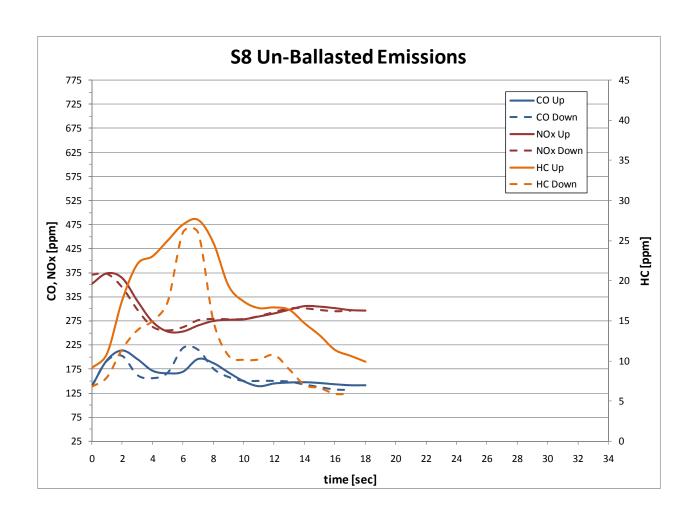












### **APPENDIX C**

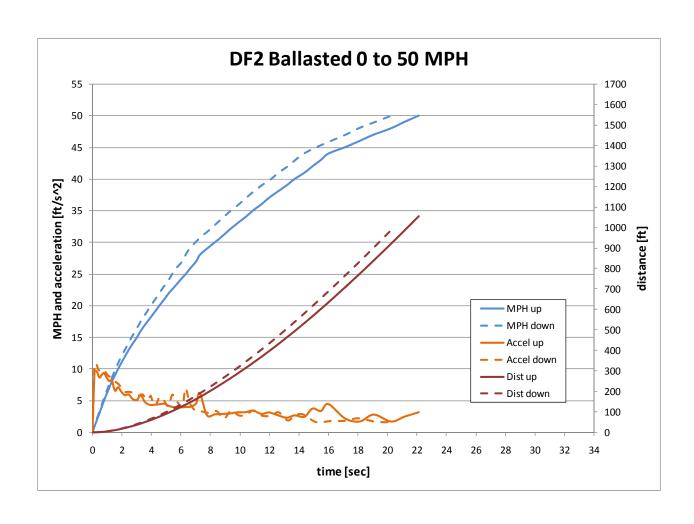
# Fischer-Tropsch Synthetic Fuels Evaluations HMMV Test Track Evaluation

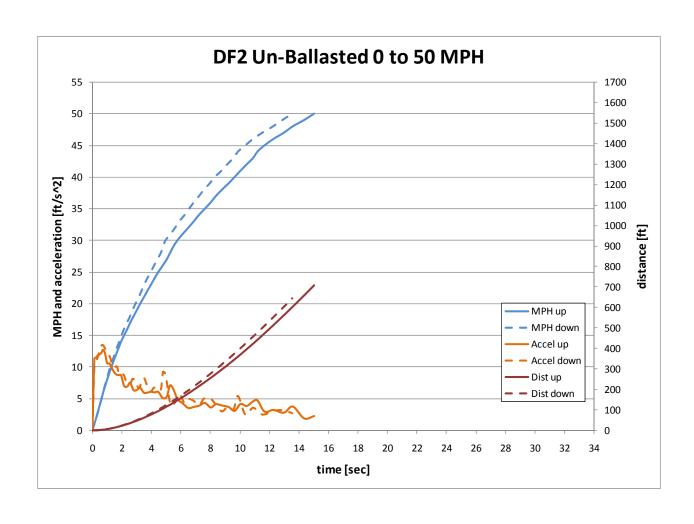
Work Directive No. 23, Task XI

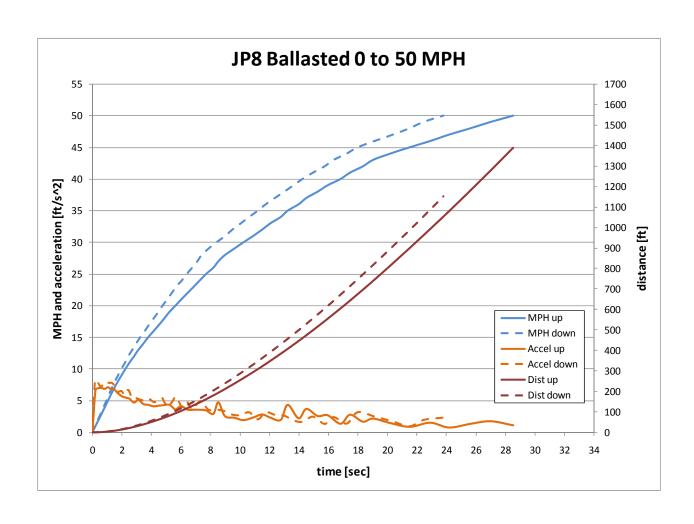
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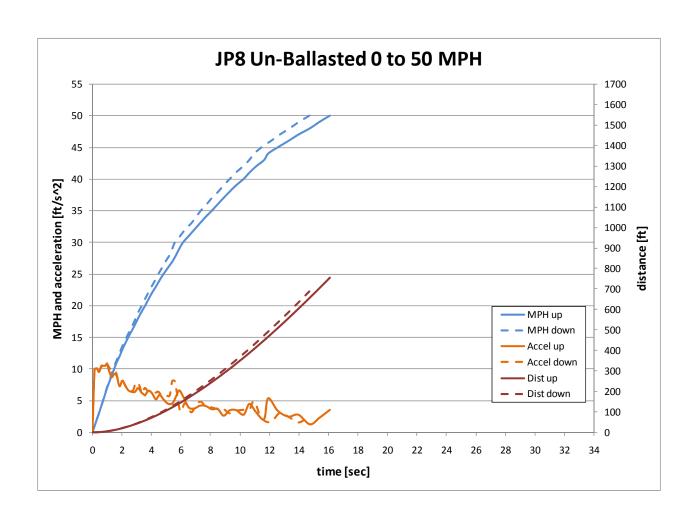
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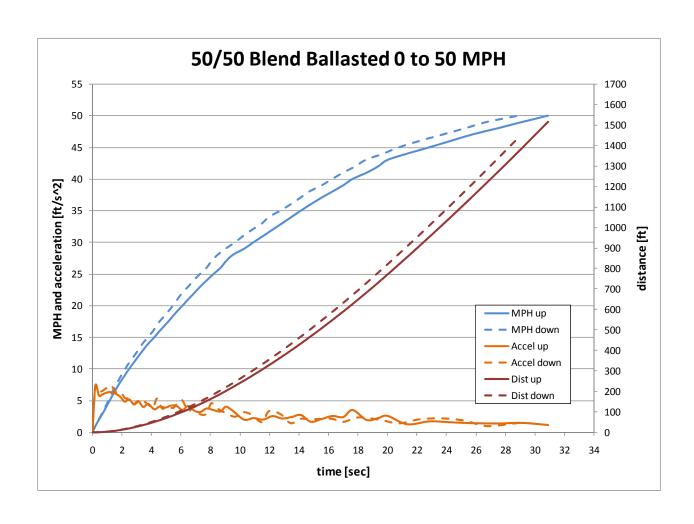
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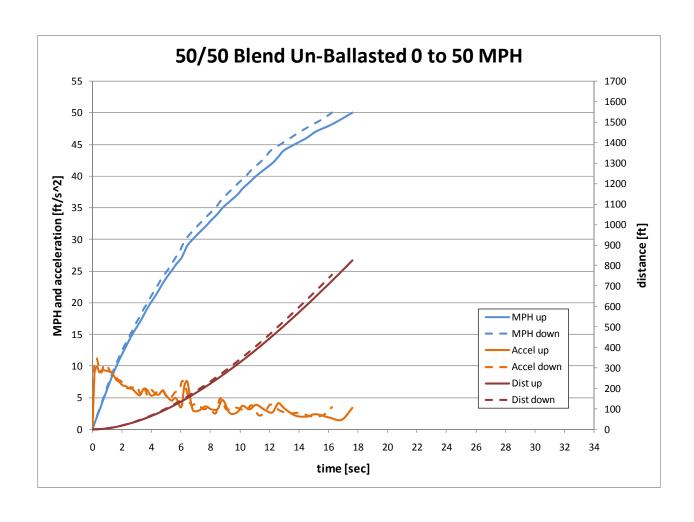


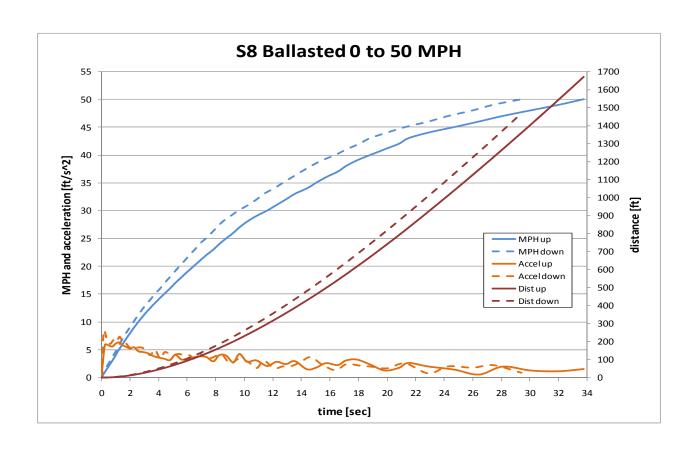


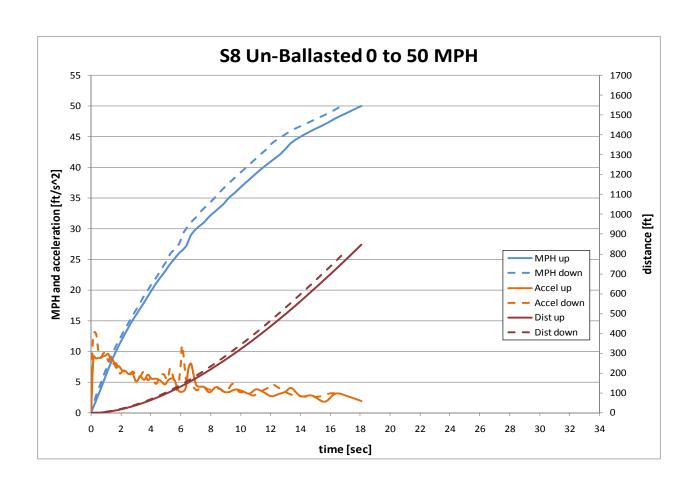












### **APPENDIX D**

## Fischer-Tropsch Synthetic Fuels Evaluations HMMV Test Track Evaluation

Work Directive No. 23, Task XI

**Stanadyne Pump Calibration / Evaluation** 

**Conducted for** 

U.S. Army TARDEC Force Projection Technologies Warren, Michigan 48397-5000

### Stanadyne Pump Calibration / Evaluation

Pump Type : DB2831- 5149 (arctic) SN: 14763014

Test condition: HMMWV NATO Testing AL:

| PUMP RPM | Description            | Spec.          | Pre Test  | Post Test | Change | ReCalibrated |
|----------|------------------------|----------------|-----------|-----------|--------|--------------|
| 1000     | Transfer pump psi.     | 60-62 psi      | 67        | 67        | 0      | 62           |
|          | Return Fuel            | 225-375 cc     | 370       | 422       | 52     | 280          |
|          | Fuel Delivery          | 56 cc. Max.    | 55        | 55        | 0      | 55           |
| 350      | Low Idle               | 12-16 cc       | 13.5      | 10.5      | -3     | 14           |
|          | Housing psi.           | 8-12 psi       | 9.5       | 9.5       | 0      | 5            |
|          | Cold Advance Solenoid  | 0-1 psi.       | 0.5       | 1         | 0.5    | 1            |
| 1700     | Fuel Delivery          | 49 - 52 cc     | 50        | 51        | 1      | 50           |
|          | Advance                | 3.5 - 4.5 deg. | 3.75      | 3.77      | 0.02   | 3.83         |
| 1750     | Fuel Delivery          | 45 cc. min.    | 51        | 51        | 0      | 52           |
| 1825     | Fuel Delivery          | 31.5 cc min.   | 35        | 21        | -14    | 39           |
| 1600     | Face Cam Fuel delivery | 21.5 - 23.5 cc | 22        | 22        | 0      | 22           |
|          | Advance                | 4 - 6 deg.     | 4.75      | 4.35      | -0.4   | 4.35         |
| 750      | De-Energize E.S.O.     | 4 cc max.      | 0.5       | 0.5       | 0      | 0.5          |
| 1800     | Fuel Delivery          | Record         | 41        | 27        | -14    | 47           |
|          | Transfer pump psi.     | Record         | 100       | 98        | -2     | 95           |
|          | Housing psi.           | Record         | 10        | 8.5       | -1.5   | 10           |
| 1950     | High Idle              | 15 cc max.     | 5         | 1         | -4     | 6            |
|          | Transfer pump psi.     | 125 psi max.   | 115       | 110       | -5     | 112          |
| 200      | Fuel Delivery          | 43 cc min.     | 50        | 50        | 0      | 48           |
|          | Shut-Off               | 4 cc max.      | 0         | 0.5       | 0.5    | 0.5          |
| 75       | Fuel Delivery          | 28 cc min.     | 40        | 44        | 4      | 40           |
|          | Transfer pump psi.     | 16 psi min.    | 27        | 27        | 0      | 29           |
|          | Air Timing             | -1 deg. (+/5)  | -1        | -1        | 0      | -1           |
|          | Fluid Temp. Deg. C     |                | nr        | nr        |        | nr           |
|          | Date                   |                | 2/25/2009 | 5/28/2009 |        | 6/1/2009     |

The shaded boxes show where the pump is operating out of specification.

### **APPENDIX E**

## Fischer-Tropsch Synthetic Fuels Evaluations HMMV Test Track Evaluation

Work Directive No. 23, Task XI

### Elapsed Photos Showing the HMMWV Driving around SwRI Campus and the Test Track

**Conducted for** 

U.S. Army TARDEC Force Projection Technologies Warren, Michigan 48397-5000





